

## Reference Evapotranspiration Estimation Using Locally Adjusted Coefficient of Angstrom's Radiation Model in an Arid-Cold Region

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### ABSTRACT

Acceptable estimation of reference Evapotranspiration ( $ET_0$ ) values by the Penman-Monteith FAO (PM FAO) equation requires accurate solar radiation ( $R_s$ ) data.  $R_s$  values could be estimated using the Angstrom's radiation model. The aim of this study was to determine the  $a_s$  and  $b_s$  coefficient (as Angstrom's parameters) for the Ardabil plain as an arid and cold region. Angstrom's radiation model and PM FAO equation were calibrated for the study area, by optimizing the  $a_s$  and  $b_s$  parameter using Generalized Reduced Gradient (GRG) method. Measured  $R_s$  data were collected from the Ardabil Synoptic Station and measured  $ET_0$  data were determined using three lysimeters that were installed at the Hangar Research Station. Calibrated results showed that optimized  $a_s$  and  $b_s$  values were 0.117 and 0.384, respectively. Compared to the original models, errors including RMSE, AE and RE values were decreased and fitted parameters including  $R^2$  and regression line slope ( $m$ ) were improved in the calibrated models. The GMER values for the original models showed that Angstrom's radiation model overestimated the  $R_s$  values and PM FAO equation underestimated the  $ET_0$  values. Locally calibrated models estimated  $R_s$  and  $ET_0$  values better than the original one. Nash-Sutcliffe efficiency coefficient (NSE) values proved that  $R_s$  and  $ET_0$  estimation by the original models were not satisfactory, but were acceptable in the case of the calibrated models. However, calibration of Angstrom's radiation model and PM FAO equation is necessary for each region.

**Keywords:** Penman-Monteith, Model calibration, Validation, Lysimeter, Ardabil

### INTRODUCTION

Accurate estimates of actual evapotranspiration are a prerequisite for real-time irrigation forecasting (Doorenbos and Kassam, 1979). Lysimeters have been used to analyze precipitation ( $P$ ), drainage water, root water uptake, and to determine actual evapotranspiration ( $ET_a$ ) (Young *et al.*, 1996; Bakhtiari *et al.*, 2011). Specific devices and lysimeters are required to determine evapotranspiration, various physical parameters, and soil water balance (Allen *et al.*, 2006). The estimation of crop evapotranspiration ( $ET_c$ ) often involves calculating the reference evapotranspiration ( $ET_0$ ) (Xu *et al.*, 2012). Reference evapotranspiration (grass) is defined as the

evapotranspiration rate from a hypothetical crop with an assumed height of 0.12 m, a fixed surface resistance of  $70 \text{ s.m}^{-1}$ , and an albedo of 0.23. The only factors affecting  $ET_0$  are climatic parameters. Therefore,  $ET_0$  is a climatic parameter that can be computed from weather data (Allen *et al.*, 1998). The FAO Penman-Monteith combination equation (FAO-56 PM Equation) was proposed as a standard method for estimating reference evapotranspiration, and for evaluating other equations. It is accepted worldwide as the optimum method and the standard for evaluating other methods (e.g., Jacovides and Kontonyiannis, 1995; Antonio, 2004; Hossein *et al.*, 2004; Xu and Chen, 2005; López-Urrea *et al.*, 2006; Trajkovic, 2007; Meshram *et al.*, 2010; da Silva *et al.*, 2011; Mohawesh, 2011).

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From the original equations of Penman-Monteith and the aerodynamic and surface resistance, the FAO Penman-Monteith method to estimate  $ET_0$  can be derived as follows (Temesgen *et al.*, 2005):

$$ET_0 = \frac{0.408 \Delta (R_n - G) + \gamma \frac{900}{T + 273} u_2 (e_s - e_a)}{\Delta + \gamma (1 + 0.34 u_2)} \quad (1)$$

Where,  $ET_0$  is the reference evapotranspiration [ $\text{mm day}^{-1}$ ],  $R_n$  is the net radiation at the crop surface [ $\text{MJ m}^{-2} \text{day}^{-1}$ ],  $G$  is the soil heat flux density [ $\text{MJ m}^{-2} \text{day}^{-1}$ ],  $T$  is the mean daily air temperature at 2 m height [ $^{\circ}\text{C}$ ],  $u_2$  is the wind speed at 2 m height [ $\text{m s}^{-1}$ ],  $e_s$  is the saturation vapor pressure [ $\text{kPa}$ ],  $e_a$  is the actual vapor pressure [ $\text{kPa}$ ],  $(e_s - e_a)$  is the saturation vapor pressure deficit [ $\text{kPa}$ ],  $\Delta$  is the slope vapor pressure curve [ $\text{kPa } ^{\circ}\text{C}^{-1}$ ], and  $\gamma$  is the psychrometric constant [ $\text{kPa } ^{\circ}\text{C}^{-1}$ ].

The FAO-56 PM is a physically based approach which requires measurements of air temperature, relative humidity, solar radiation, and wind speed. Net radiation,  $R_n$ , is the most important parameter in the calculation of  $ET_0$  by FAO-56 PM (Xu, *et al.*, 2009). Solar radiation,  $R_s$ , can be calculated with the Angstrom formula, which relates solar radiation to extraterrestrial radiation and relative sunshine duration as:

$$R_s = \left( a_s + b_s \frac{n}{N} \right) R_a \quad (2)$$

Where,  $R_s$  is the solar or shortwave radiation [ $\text{MJ m}^{-2} \text{day}^{-1}$ ],  $n$  is the actual duration of sunshine [hour],  $N$  is the maximum possible duration of sunshine or daylight hours [hour],  $\frac{n}{N}$  is the relative sunshine duration [-],  $R_a$  is the extraterrestrial radiation [ $\text{MJ m}^{-2} \text{day}^{-1}$ ],  $a_s$  is the regression constant, expressing the fraction of extraterrestrial radiation reaching the earth on overcast days ( $n = 0$ ),  $a_s + b_s$  is the fraction of extraterrestrial radiation reaching the earth on clear days ( $n = N$ ). Depending on atmospheric conditions (humidity, dust) and solar declination (latitude and month), the Angstrom's values  $a_s$  and  $b_s$  will vary. Where no actual solar radiation data are available and no

calibration has been carried out for improving  $a_s$  and  $b_s$  parameters, the values  $a_s = 0.25$  and  $b_s = 0.50$  are recommended (Allen *et al.*, 2006). Values for  $R_a$  and  $N$  for different latitudes are listed in FAO Irrigation and Drainage Paper No. 56, or could be calculated from related equations. The actual duration of sunshine,  $n$ , is recorded with a Campbell Stokes sunshine recorder. Net radiation is measured in some meteorological stations such as Ardabil station. Estimation of various  $R_s$  using equation (2), can affect  $ET_0$  values change, because the hypothetical surface with uniform albedo of 0.23 can't be realized in the measurement of net radiation in all climate stations. Based on solar radiation determined with different regimes of  $a_s$  and  $b_s$ , influence on calculation of  $ET_0$  have been investigated (Xu *et al.*, 2006). Xu *et al.* (2009) concluded that errors in  $ET_0$  caused by different values of  $a_s$  and  $b_s$  are not neglectable. In stations with solar radiation measurement, it is possible and necessary to evaluate and estimate the Angstrom's coefficients, to calculate solar radiation and hence  $ET_0$ . Many studies have been done on the estimation of reference plant evapotranspiration by various methods. Gocic' *et al.* (2015) indicated that SVM-W (support vector machine-wavelet) is the best methodology for prediction of  $ET_0$ , whereas SVM-Wavelet and SVM-FFA (support vector machine-firefly algorithm) models have higher correlation coefficient as compared to ANN (artificial neural network) and GP (genetic programming) computational methods. Petkovic' *et al.* (2015) used the neuro-fuzzy inference system (ANFIS) for selection of the most influential reference evapotranspiration ( $ET_0$ ) parameters. They concluded that, among the input variables, sunshine hours, actual vapor pressure, and minimum air temperature are the most influential for  $ET_0$  estimation. In another research, Petkovic' *et al.* (2016) showed that the radial basis function network with particle swarm optimization (RBFN-PSO) had better

statistical characteristics than radial basis function network with back propagation (RBFN-BP) and could be helpful for the  $ET_0$  estimation. Shamshirband *et al.* (2016) indicated that combination of adaptive neuro fuzzy interference system (ANFIS) and cuckoo search algorithm (CSA) could be used for  $ET_0$  estimation with high reliability. Gocic *et al.* (2016) used the extreme learning machine (ELM) for estimating monthly reference evapotranspiration ( $ET_0$ ) in two weather stations including Nis and Belgrade, Serbia. Results showed that adjusted Hargreaves model was found to be superior in modeling monthly  $ET_0$  than the Priestley-Taylor and Turc models.

The main aim of this study was to investigate the effect of different values of Angstrom's coefficients for estimation of solar radiation and  $ET_0$  in Ardabil plain as an arid and cold region, using lysimeter data.

## MATERIALS AND METHODS

### Site Description

This study was conducted in Ardabil plain ( $38^\circ, 10'$  to  $38^\circ, 15'$  N,  $48^\circ, 15'$  to  $48^\circ, 20'$  E and 1350 m elevation above the sea). The Ardabil climate station ( $38^\circ, 15'$  N,  $48^\circ, 17'$

E) was selected as a typical climate station in an arid and cold region in northeast of Iran (Figure 1). Experimental site was located at Hangar Farm of Mohagheh Ardabili University. The annual mean precipitation rate, average minimum monthly temperature, and average maximum monthly temperature through 1995 to 2015 were obtained as 280.9 mm,  $2.4^\circ\text{C}$ , and  $15.07^\circ\text{C}$ , respectively.

For the following two reasons, the length of the study period was considered 81 days.

1. The growth period of the grass is 45 days and then the cutting period. Thus, the earliest 45 days were the growth period, and the end 36 days were the cutting period.
2. Snow in early November (Aban) led to the completion of the study period.

At the study period, the averages of minimum ( $T_{\min}$ ) and maximum air temperature ( $T_{\max}$ ), daily sunshine hour ( $n$ ), actual relative humidity ( $RH_a$ ), solar radiation ( $R_s$ ), and wind speed ( $v$ ) were  $10.43^\circ\text{C}$ ,  $25.04^\circ\text{C}$ , 8.85 hr, 65.31%, 5.25 mm/day and 3.33 m/s, respectively. Statistical parameters of the observed meteorological data from 22 July, 2014, to 10 October, 2014, (calibration and validation periods) are listed in Table 1.

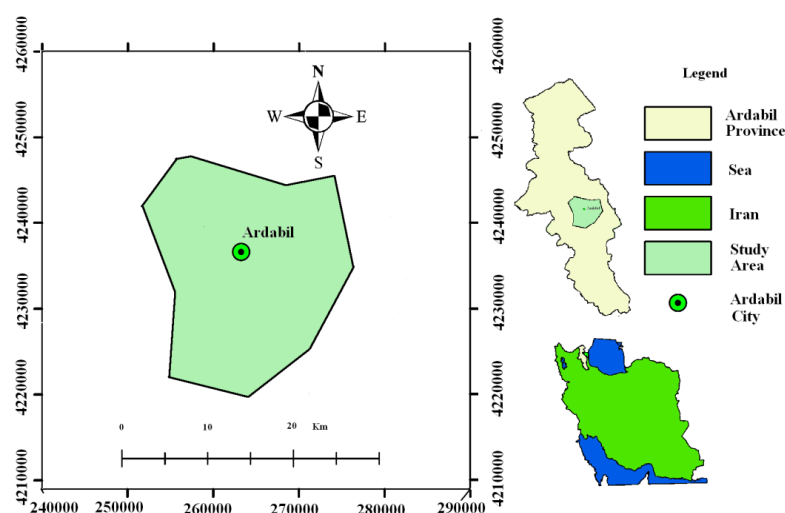


Figure 1. Location of study area.



**Table 1.** Statistics of observed meteorological data.

Statistic parameters		$T_{\max}$ (°C)	$T_{\min}$ (°C)	$T_{\text{avg}}$ (°C)	$RH_a$ (%)	$R_s$ (MJ/m <sup>2</sup> .day)	n (hr)	$u_2$ (m/s)
Calibration period (22 July 2014 to 13 September 2014)	Maximum	40.4	16.2	29.9	96	7.63	13	7.37
	Minimum	15.4	6.2	12.6	22.6	0.81	0.2	1.25
	Average	26.43	11.4	19.1	61.58	6.17	9.89	3.46
	Cv (%)	19.53	20.43	16.61	27.51	23.64	34.48	42.2
Validation period (14 September 2014 to 10 October 2014 )	Maximum	29	16.2	20.2	97.12	5.93	11.2	9.12
	Minimum	10.4	3.4	8.5	37.62	1.59	0.2	0.62
	Average	22.26	8.5	14.83	72.76	4.09	6.75	3.06
	Cv (%)	37.16	20.56	18.72	19.27	33.17	46.05	70.2

### Lysimeters Characteristics

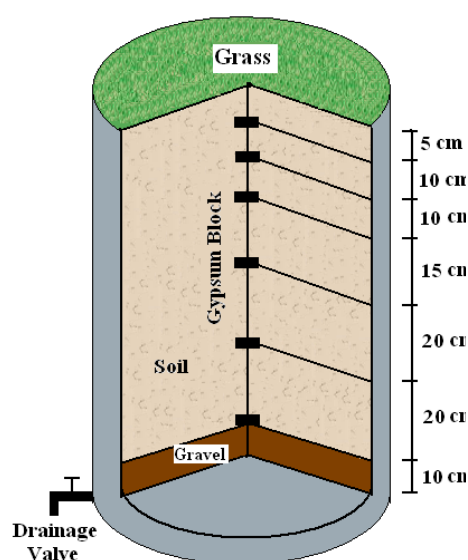
Three lysimeters were installed to determine the water balance equation, estimate reference evapotranspiration, and calibrate Angstrom's Radiation Model (determining the  $a_s$  and  $b_s$  coefficients) in Hangar Farm site. Sectional drawing of a lysimeter is illustrated in Figure 2. Dimensions of each lysimeter were 60 cm diameter and 90 cm height. To measure the water content changes in each lysimeter, 6 sensors (gypsum block) were installed at depth of 5, 15, 25, 40, 60 and 80 cm, from the soil surface. To measure soil moisture, it is necessary that the resistance of the gypsum

blocks is measured, then, the values of the block resistance are converted to soil moisture using a calibration curve. Blocks resistance data was measured at 10:00 AM and 18:00 PM every day using an ELE-MC-302 soil moisture instrument. Drained water was collected in a drainage tank located under the lysimeters and was measured two times every day, the same as blocks resistance.

In the lysimeters, grass was planted, as reference crop, on 22 July, 2015, and irrigated every 3 days, according to the lysimeters soil type. Given that the purpose of this study was to measure potential evapotranspiration, the irrigation interval was chosen to avoid plant stress. For irrigation intervals of 3 days, soil type did not create restrictions. Figure 2 illustrates schematic of lysimeters and its devices. To calculate soil water storage, lysimeters soil was divided into 6 layers, including the depth of 0-10, 10-20, 20-32.5, 32.5-50, 50-70, and 70-90 cm, according to the depth of installation of gypsum blocks (at depths of 5, 15, 25, 40, 60 and 80 cm). The value of the soil water content was obtained for each of the layers using the gypsum blocks data. To determine some soil physical and hydraulic properties, three disturbed and three undisturbed soil sample were taken. The total soil water storage was determined by the sum of storage in each of the considered layers (Equation 3) (Feltrin *et al.*, 2011):

$$S = \int_0^L \theta dz \approx \sum_{i=1}^n \theta \Delta z = \theta L \quad (3)$$

Where,  $S$  is the soil water storage (mm),  $\theta$  is the volumetric soil water content (cm<sup>3</sup>/cm<sup>3</sup>),  $L$



**Figure 2.** Sectional drawing of a lysimeter used for  $ET_0$  measurement.

is the total soil depth (mm), and  $n$  is the number of layer. Thus, the change in soil water storage was determined by the difference between the values of the soil water content obtained in the final and initial time of each period (daily period), using equation 4:

$$\Delta S = S_f - S_i \quad (4)$$

Where,  $\Delta S$  is the change in soil water storage (mm),  $S_i$  and  $S_f$  are the initial and final soil water storage (mm), respectively. The water balance equation of the lysimeters was used to calculate the grass evapotranspiration ( $ET_0$ ). The evapotranspiration was obtained by the difference between the soil water inputs and outputs (Equation 5):

$$ET = P - D + \Delta S \quad (5)$$

Where,  $ET$  is the evapotranspiration (mm),  $P$  is the rainfall (mm),  $D$  is the drainage (mm), and  $\Delta S$  is the change in soil water storage (mm).

#### PM FAO Equation: Calibration and Validation

The coefficients  $a_s$  and  $b_s$ , with the original values of 0.25 and 0.5, respectively, should be determined according to the local calibration. Based on observed evapotranspiration data from 22 July to 13 September, 2014, local calibration was performed to determine the values of coefficients  $a_s$  and  $b_s$  through nonlinear multiple regression for the  $ET_0$  calculated using the FAO-56 PM equation and measured  $ET_0$ . The nonlinear multiple regressions were realized using the Solver extension of Excel software with Generalized Reduced Gradient method (GRG). The locally calibrated PM FAO equation was validated for the data from 14 September to 10 October 2014, by comparing the results with the measured data. For evaluation of the  $ET_0$  calculated by PM FAO equation relative to the measured data, firstly, the calculated and measured data were plotted around the 1:1 line. Linear regressions with zero interception were made, and slopes and determination coefficients ( $R^2$ ) were calculated.

#### Statistical Analysis

In the present study, root mean square error (RMSE), average absolute errors (AE), Nash-Sutcliffe efficiency coefficient (NSE) and relative error (RE), were used to evaluate the Angstrom's radiation model (in estimation of  $R_s$ ) and PM FAO equation (in estimation of  $ET_0$ ), derived from different values of  $a_s$  and  $b_s$  coefficient. Statistical parameters were calculated using the following expressions:

$$RMSE = \sqrt{\frac{1}{n} \sum_{i=1}^n (O_i - P_i)^2} \quad (6)$$

$$AE = \frac{1}{n} \sum_{i=1}^n (|O_i - P_i|) \quad (7)$$

$$NSE = 1 - \frac{\sum_{i=1}^n (O_i - P_i)^2}{\sum_{i=1}^n (O_i - \bar{O})^2} \quad (8)$$

$$RE = \frac{\sum_{i=1}^n |O_i - P_i|}{\sum_{i=1}^n O_i} \times 100 \quad (9)$$

Results were categorized into four groups by analysis of the relative error using the following criteria (Xu *et al.*, 2009):

RE < 10% indicates very good, 15% > RE > 10% indicates good, 20% > RE > 15% indicates acceptable, and RE > 20% indicates poor result.

To evaluate the overestimation or underestimation of Angstrom's radiation model and PM FAO equation, geometric mean error ratio (GMER) were also used as follows:

$$GMER = \exp\left(\frac{1}{n} \sum_{i=1}^n \ln\left(\frac{O_i}{P_i}\right)\right) \quad (10)$$

If predicted values were equal to observed values, GMER reach unity. A GMER > 1 indicates overestimation and GMER < 1 shows underestimation of the mentioned values (Wagner *et al.*, 2001). In all evaluation equations (Equations 6 to 10),  $O_i$  and  $P_i$  represent the observed and predicted data, respectively.

## RESULTS AND DISCUSSION

### Soil Properties and Water Balance

Results from the granulometric analysis of the samples collected at the site of the lysimeters installation are shown in Table 2. The amount of sand percentage, which was over 60% of the total in all lysimeters, caused soil available water to decrease and drained



water to increase. Some soil hydraulic properties that determine the soil available water are illustrated in Table 3. Total soil available water was 140 mm/m, as calculated from the field capacity and permanent wilting point water content. Volumetric soil water content changes in depth of 5, 15, 25, 40, 60 and 80 cm and water storage in the period are shown in Figure 3. In this figure, increase in water content indicates irrigation (wetting trend) and decrease in the water content indicates soil water extraction (drying trend). Because evaporation is more intense in the surface layer, for the depth of 5 and 15 cm, water content changes more rapidly than other depths. The positive and negative values of water storage represent the frequent

addition and depletion of water in the lysimeters.

### Evaluation of Estimated $R_s$ and $ET_0$ during the Entire Period

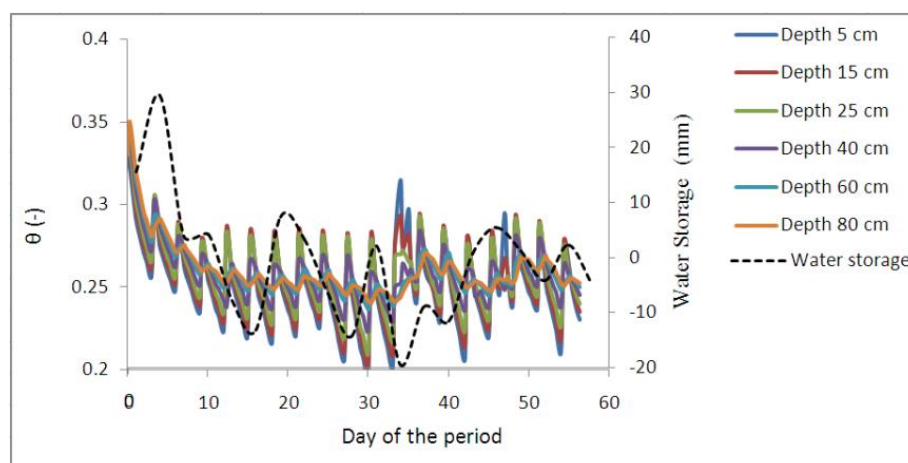
Daily radiation values estimated by the Angstrom's radiation model and daily  $ET_0$  values estimated by the PM FAO equation compared with the measured data are illustrated in Figures 4 and 5, respectively, in which  $R_s$  and  $ET_0$  values are also shown around the 1:1 (one to one) line. Regression equation has been derived between the measured and estimated  $R_s$  and  $ET_0$  with zero interception. The radiation values in warm

**Table 2.** Some soil physical properties of the study site.

Parameter	Particle Density (gr/m <sup>3</sup> )	Bulk density (gr/m <sup>3</sup> )	Total Porosity (%)	Granulometry			Texture Class
				Clay (%)	Silt (%)	Sand (%)	
Mean	2.4235	1.225	49.45	6.67	31.47	61.87	Sandy Loam
Standard Deviation	0.0456	0.0925	3.203	0.9428	2.494	2.944	
CV	0.02	0.07	0.06	0.14	0.08	0.04	

**Table 3.** Some soil hydraulic properties of the study site.

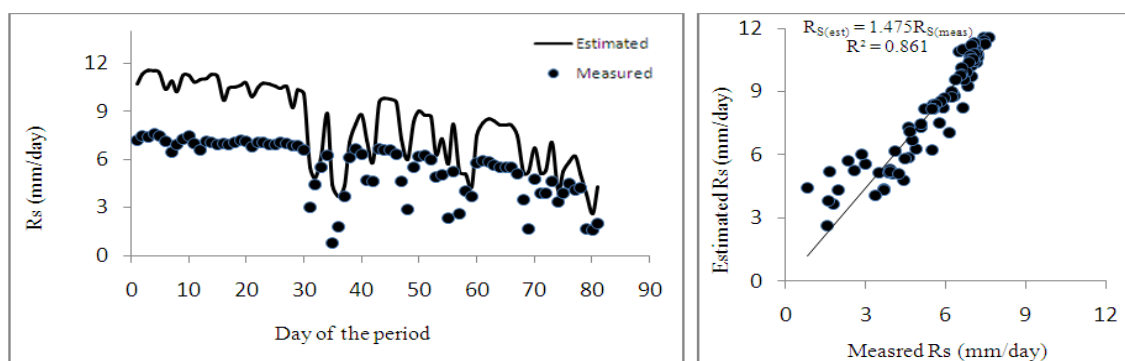
$\theta_r$ (cm <sup>3</sup> /cm <sup>3</sup> )	$\theta_{FC}$ (cm <sup>3</sup> /cm <sup>3</sup> )	$\theta_s$ (cm <sup>3</sup> /cm <sup>3</sup> )	$K_s$ (cm/day)	$\alpha$ (-)	$n$ (-)
0.1226	0.2626	0.4945	281.6	0.01556	1.76466



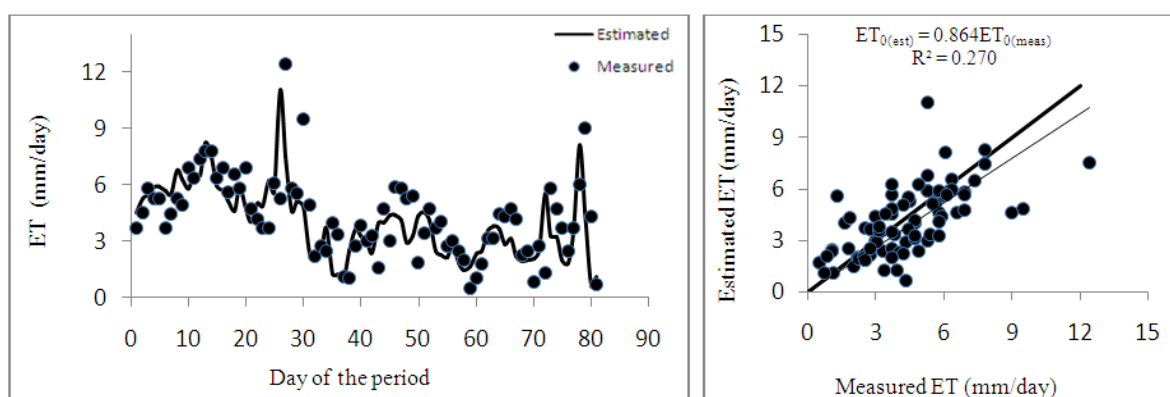
**Figure3.** Volumetric soil water content changes in depth of 5, 15, 25, 40, 60 and 80 cm and daily water storage.

days are greater than cold days. According to Figures 4 and 5, measured daily radiation values fluctuated between 0.81 and 7.63 mm/day and measured evapotranspiration ( $ET_0$ ) values fluctuated between 0.54 and 12.42 mm/day. Before local calibration and validation (with  $a_s=0.25$  and  $b_s=0.75$ , recommended by FAO), the PM FAO model had a high error and therefore the model must be calibrated and validated locally. Statistical

parameters of Angstrom's radiation model and PM FAO equation estimation are showed in Table 4. In both  $R_s$  and  $ET_0$  estimation with  $a_s$  and  $b_s$  coefficient recommended by FAO, results are not satisfactory. The RMSE, AE, and RE, which explain the error between the measured and estimated parameters, have high values, indicating that Angstrom's radiation model and PM FAO equation require calibration in each region.



**Figure 4.** Daily radiation values ( $R_s$ ) estimated by the Angstrom's radiation model compared with the measured data, before local calibration (during the entire period and around the 1:1 line)



**Figure 5.** Daily  $ET_0$  values estimated by the PM FAO equation compared with the measured data, before local calibration (during the entire period and around the 1:1 line)

**Table 4.** Statistical parameters of Angstrom's radiation model and PM FAO equation before local calibration.

Angstrom's radiation model			PM FAO equation		
Parameter	Value	Explanation	Parameter	Value	Explanation
$R^2$ (-)	0.861	Acceptable	$R^2$ (-)	0.27	Non acceptable
M (line slope) (-)	1.475	Non acceptable	M (line slope) (-)	0.864	Non acceptable
RMSE (mm/day)	2.882	High	RMSE (mm/day)	1.778	High
AE (mm/day)	2.688	High	AE (mm/day)	1.342	High
NSE (-)	-0.114	Non satisfied	NSE (-)	0.291	Non satisfied
RE (%)	49.061	Poor	RE (%)	30.96	Poor
GMR (-)	0.656	Overestimated	GMR (-)	1.054	Underestimated





Value of  $R^2$  is acceptable for radiation model, but it is small for PM FAO equation. For  $ET_0$  values, points are very far from 1:1 line. In Table 4, M values represent the slope of the fitted line between the measured and estimated data with zero interception. The value of M close to one indicates high accuracy of the model. For both models, Nash-Sutcliffe efficiency coefficient (NSE) values are not acceptable, because NSE of both models is less than 0.36. This parameter is better for  $ET_0$  estimation than for  $R_s$  estimation. The GMER values showed that the Angstrom's radiation model overestimated the  $R_s$  values, but PM FAO equation underestimated the  $ET_0$  values.  $R_s$  overestimation and  $ET_0$  underestimation related to parameters of those equations. In the study period, the average of overestimation of  $R_s$  is 2.69 mm/day, corresponding to a relative difference of approximately 49.06 % with respect to measured  $R_s$  data. The average of underestimation of  $ET_0$  is 0.29 mm/day, corresponding to a relative difference of approximately 6.66% with respect to measured  $ET_0$  data. These overestimation and underestimation could not be ignored.

### Local Calibration and Validation

Local calibration of Angstrom's radiation model and then PM FAO equation was carried out using two third of the entire data, including 54 days. Calibration was performed by optimization of Angstrom's  $a_s$  and  $b_s$  coefficients using the Solver extension of Excel software with Generalized Reduced Gradient (GRG) method. Local  $a_s$  and  $b_s$  coefficients were obtained equal to 0.117 and 0.384, respectively. To validate the models, values of  $R_s$  and  $ET_0$ , were estimated using calibrated radiation and  $ET_0$  equation for one third of the entire data, including 27 days. Coefficients  $a_s$  and  $b_s$  in the current study are much smaller than the original value suggested by Allen *et al.* (2006) and Xu *et al.* (2009).

### Evaluation of Estimated $R_s$ and $ET_0$ during the Calibration and Validation Periods

Coefficients  $a_s$  and  $b_s$  were estimated in Ardabil plain as an arid-cold region to improve results of Angstrom's radiation model and PM FAO equation for estimation of  $R_s$  and  $ET_0$ . In the calibration step, the values of  $a_s$  and  $b_s$  were determined as 0.117 and 0.384 for the study region. The  $R_s$  and  $ET_0$  values were re-calculated with these new values of  $a_s$  and  $b_s$ . For calibration step, estimated daily radiation values compared with those measured one are illustrated in Figure 6. Estimated daily  $ET_0$  values compared with the measured data, also, are illustrated in Figure 7. The statistical parameters of the Angstrom's radiation model and PM FAO equation, related to the calibration step, are given in Table 5.

Validation of the model was carried out with 27 data. The values obtained from the calibration step, were used in the validation step. The values of  $ET_0$  and  $R_s$  obtained in the validation step are shown in Figures 8 and 9, respectively. The statistical parameters of the Angstrom's radiation model and PM FAO equation, related to the validation step, are also given in Table 6. Comparing the results of the original Angstrom's radiation model and original PM FAO equation with those locally calibrated showed that the errors (RMSE, AE and RE) were decreased and the fitted parameters (M,  $R^2$  and NSE) were improved. In estimation of  $R_s$ , the RMSE, AE and RE decreased 2.427 mm/day, 2.381 mm/day and 42.041%, respectively. In estimation of  $ET_0$ , the RMSE, AE and RE also decreased 1.01mm/day, 0.895 mm/day and 16.246%, respectively.

The  $R^2$  values in validation step were increased compared to before calibration from 0.861 to 0.935 for  $R_s$  model and from 0.27 to 0.877 for  $ET_0$  equation, indicating that the  $ET_0$  estimation improved highly. The GMER values in different stages proved that underestimation or overestimation of  $R_s$  and  $ET_0$  decreased in locally calibrated models

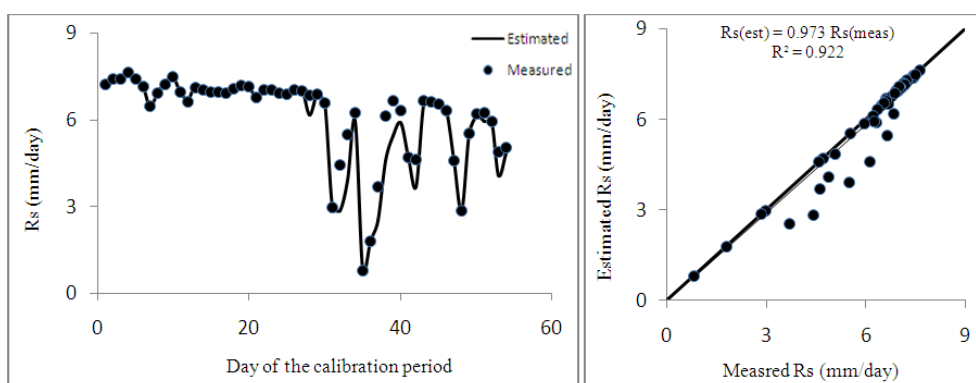


and caused the line slopes (M) reach near unity and the points were perched in around the 1:1 line in Figures 6 to 9. If NSE values reach values more than 0.36, the efficiency of the model will be satisfactory. In locally calibrated models, compared to the original models, the NSE values were increased from -0.114 to 0.887 in  $R_s$  model and from 0.291 to 0.809 in  $ET_0$  model. The RE value and its criteria showed that the original Angstrom's

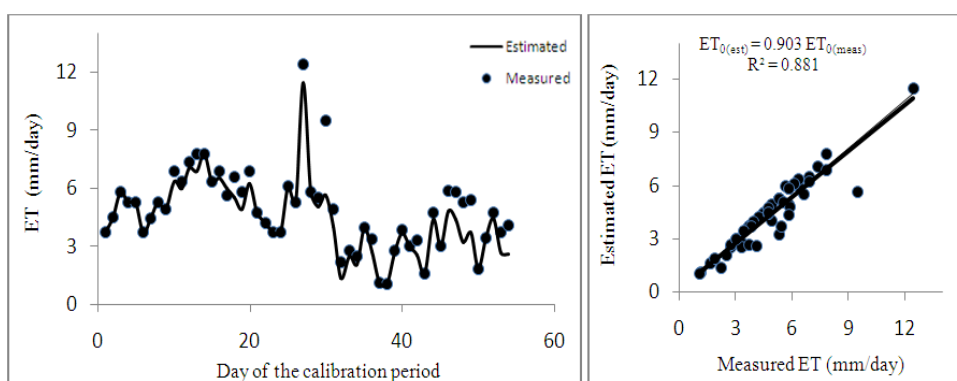
radiation model and the original PM FAO equation have poor accuracy, whereas the locally calibrated ones have very good and good accuracy, respectively.

## CONCLUSION

For an arid-cold region, the Angstrom's radiation model and the PM FAO equation



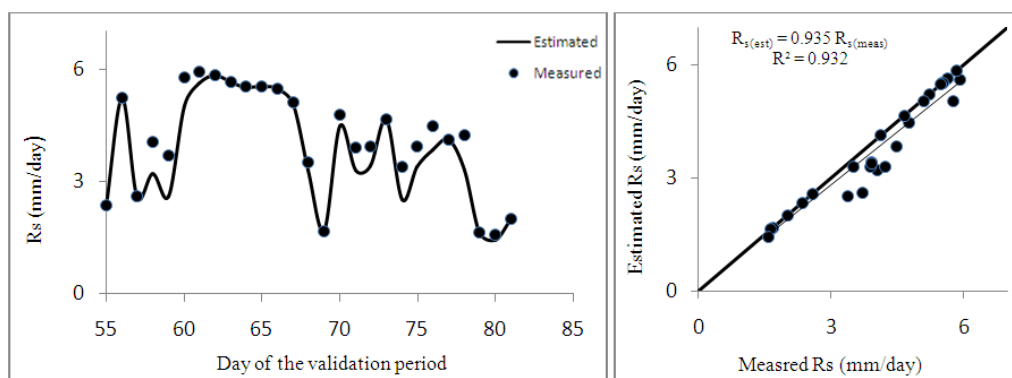
**Figure 6.** Daily  $R_s$  values estimated by the locally calibrated Angstrom's radiation model compared with the measured data (during the calibration period and around the 1:1 line)



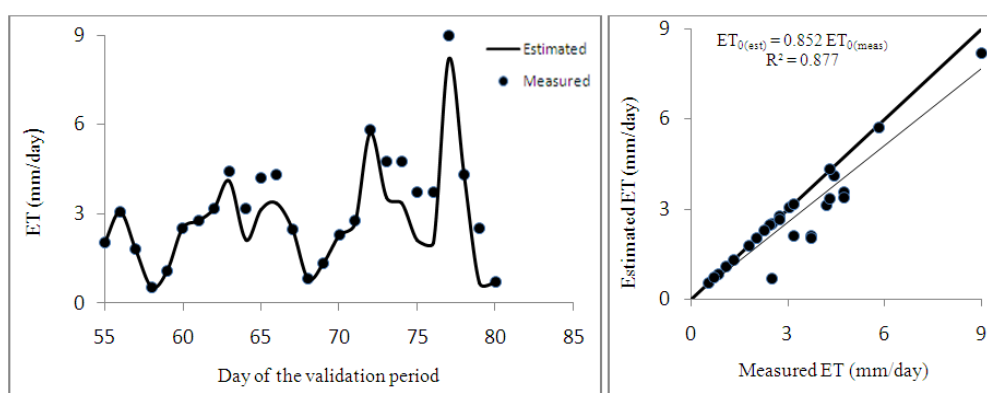
**Figure 7.** Daily  $ET_0$  values estimated by the locally calibrated PM FAO equation compared with the measured data (during the calibration period and around the 1:1 line)

**Table 5.** Statistical parameters of locally calibrated Angstrom's radiation model and PM FAO equation in the calibration stage.

Angstrom's radiation model			PM FAO equation		
Parameter	Value	Explanation	Parameter	Value	Explanation
$R^2$ (-)	0.922	Acceptable	$R^2$ (-)	0.881	Acceptable
M (line slope) (-)	0.973	Acceptable	M (line slope) (-)	0.903	Acceptable
RMSE (mm/day)	0.483	Low	RMSE (mm/day)	0.818	Low
AE (mm/day)	0.215	Low	AE (mm/day)	0.447	Low
NSE (-)	0.891	Satisfied	NSE (-)	0.838	Satisfied
RE (%)	3.483	Very good	RE (%)	9.183	Very good
GMER (-)	1.045	Underestimated	GMER (-)	1.101	Underestimated



**Figure 8.** Comparing the estimated  $R_s$  values with the measured data in validating the locally calibrated Angstrom's radiation model



**Figure 9.** Comparing the estimated  $ET_0$  values with the measured data in validating the locally calibrated PM FAO equation

**Table 6.** Statistical parameters of locally calibrated Angstrom's radiation model and PM FAO equation in the validation stage.

Angstrom's radiation model			PM FAO equation		
Parameter	Value	Explanation	Parameter	Value	Explanation
$R^2$ (-)	0.935	Acceptable	$R^2$ (-)	0.877	Acceptable
M (line slope)	0.932	Acceptable	M (line slope) (-)	0.852	Acceptable
RMSE (mm/day)	0.455	Low	RMSE (mm/day)	0.768	Low
AE (mm/day)	0.287	Low	AE (mm/day)	0.447	Low
NSE (-)	0.887	Satisfied	NSE (-)	0.809	Satisfied
RE (%)	7.02	Very good	RE (%)	14.714	Good
GMER (-)	1.083	Underestimated	GMER (-)	1.171	Underestimated

with original recommended angstrom's coefficients were evaluated. The capabilities to estimate  $R_s$  and  $ET_0$  values were examined using some statistical parameters. Both original models had low accuracy in estimation of  $R_s$  and  $ET_0$  values. Originals Angstrom's radiation model overestimated and original PM FAO equation

underestimated the values of daily  $R_s$  and  $ET_0$ , respectively. Therefore, local calibration of both models was performed in Ardabil plain using the measured  $R_s$  and  $ET_0$  values. Three lysimeters were installed at the study site to measure  $ET_0$  values. To optimize the  $a_s$  and  $b_s$  parameters, the GRG optimization method from the Solver extension of Excel

software was used. To calibrate the Angstrom's radiation model and PM FAO equation,  $a_s$  and  $b_s$  coefficients were determined by using the Solver extension of Excel software. The values of  $a_s$  and  $b_s$  were determined as 0.117 and 0.384 for the study region (compared to 0.25 and 0.5 as original values). The errors of Angstrom's radiation model and PM FAO equation were decreased and the fitted parameters were increased by local calibration of the models. By using the new values of  $a_s$  and  $b_s$  (using calibrated models), the estimates for  $R_s$  and  $ET_0$  improved and the accuracy of the models increased. Therefore, the calibration of  $R_s$  and PM FAO models is essential for each region.

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## تخمین تبخیر تعرق مرجع با استفاده از ضرایب تعدیل شده محلی معادله تابش آنگستروم در یک منطقه سرد و خشک

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### چکیده

تخمین قابل قبول تبخیر تعرق مرجع ( $ET_0$ ) بوسیله رابطه پنمن مونتیث فائو نیازمند داده‌های صحیح تابش خورشیدی ( $R_s$ ) می‌باشد. مقادیر  $R_s$  می‌تواند با استفاده از معادله تابش آنگستروم تخمین زده شود. هدف اصلی این مطالعه تعیین ضرایب  $a_s$  و  $b_s$  (به عنوان پارامترهای آنگستروم) برای دشت اردبیل به عنوان یک منطقه سرد و خشک می‌باشد. مدل تابش آنگستروم و معادله پنمن مونتیث فائو (PM FAO) با بهینه کردن مقادیر  $a_s$  و  $b_s$ ، با استفاده از روش گرادیان کاهشی تعمیم یافته (GRG)، برای منطقه مورد مطالعه واسنجی گردید. مقادیر اندازه‌گیری شده  $R_s$  از ایستگاه سینوپتیک اردبیل به دست آمد و مقادیر اندازه‌گیری شده

$ET_0$  با استفاده از سه عدد لایسمتر که در ایستگاه تحقیقاتی هانگار نصب شده بود، تعیین شد. نتایج واسنجی مدل‌ها نشان داد که مقادیر بهینه شده  $a_s$  و  $b_s$  به ترتیب برابر با ۰/۱۱۷ و ۰/۳۸۴ بود. در مدل‌های واسنجی شده برای منطقه نسبت به مدل‌های پیشنهادی اصلی، مقادیر خطا شامل RMSE، AE و RE کاهش یافت و مقادیر پارامترهای برازش مدل شامل  $R^2$  و شیب خط رگرسیون ( $m$ ) بهبود یافت. مقادیر GMER برای مدل‌های اصلی نشان داد که مدل تابش آنگستروم مقادیر  $R_s$  را بیش برآورد و مدل پنمن مونیتث مقادیر  $ET_0$  را کم برآورد می‌نمایند. مدل‌های واسنجی شده محلی مقادیر  $R_s$  و  $ET_0$  را بهتر از مدل‌های اصلی برآورد می‌نمایند. مقادیر ضریب کارآیی نش-ساتکلیف ثابت نمود که تخمین  $R_s$  و  $ET_0$  با استفاده از مدل‌های اصلی رضایت بخش نبوده اما با استفاده از مدل‌های واسنجی شده محلی رضایت بخش می‌باشد. واسنجی مدل تابش آنگستروم و معادله پنمن مونیتث فائو برای هر منطقه‌ای ضروری می‌باشد.